

# Circuits and Techniques for High-Resolution Measurement of On-Chip Power Supply Noise

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# Motivation and Challenges

- **Scaling leads to drastic reduction in required supply grid impedance.**
  - $Z \propto \text{scaling factor}^2$
  - **Achieving this low impedance (across all frequencies) is hard.**
    - **Supply noise becoming a concern even for standard digital circuits.**
- **Measuring supply noise for general chip operation is very challenging.**
  - **20 GS/s, 8-bit ADC's aren't cheap.**

# Traditional Measurement Approaches

- Previous works rely on sub-sampling oscilloscope (or similar) approaches.
  - Accurately measure repetitive waveforms.
  - Collect information about distribution of supply noise.
- Limitation: dynamics of supply noise during normal operation can't be measured.
  - Need to know distribution & spectrum of noise to characterize effects on analog or mixed signal circuits.
- **This work:** Treat supply noise as a random process, and find its spectrum by measuring autocorrelation.
  - Autocorrelation can be measured with only 2 samplers (without high sampling rate).

# Outline

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- **Random Supply Noise and Autocorrelation**
- **Measurement circuits**
- **Measurement results**
- **Conclusions**

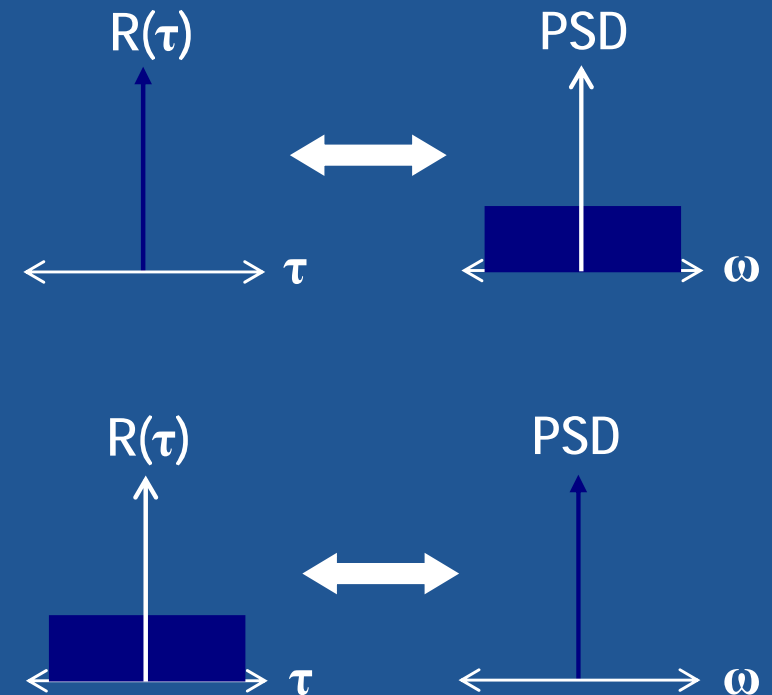
# Random Supply Noise

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- **Supply noise is basically deterministic.**
  - **But extremely complicated to calculate.**
- **Model supply noise as a random process.**
  - **Characterized by its spectrum or autocorrelation.**

# Autocorrelation

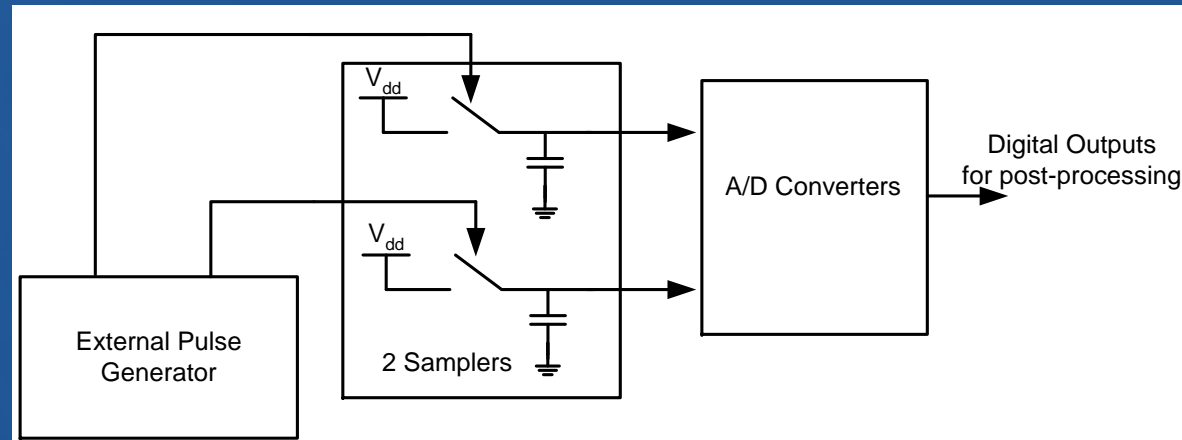
- Autocorrelation is a measure of how correlated the process is with itself at a different point in time.
  - Autocorrelation  $R(\tau) = E[V(t-\tau/2) \cdot V(t+\tau/2)]$
  - For a zero mean process,  $R(0) = \sigma^2$
- The power spectral density (PSD) of a process is the Fourier Transform of R.
  - High bandwidth – narrow R
  - Low bandwidth – wide R
- These definitions hold for stationary (time-invariant) processes.
  - Is supply noise really stationary?



# Autocorrelation (cont'd)

- Chip clocks modulate occurrence of noise events.
  - Modulation is repetitive – supply noise is cyclostationary
    - At same time point in each cycle, noise statistics are the same.
- Cyclostationary processes characterized by autocorrelation (PSD) at each point in time.
  - Stationary:  $R(\tau)$
  - Cyclostationary:  $R(t, \tau)$
- Autocorrelation is an average statistical property.
  - Don't need to know signal at every point in time – just need pairs of signal values.
  - Nyquist frequency set by **minimum**  $\tau$  (not by sampling rate).
    - Greatly reduces throughput requirements of sampling circuits.
  - For cyclostationary measurement, just need to be able to lock sampling instant to a time point in the cycle.

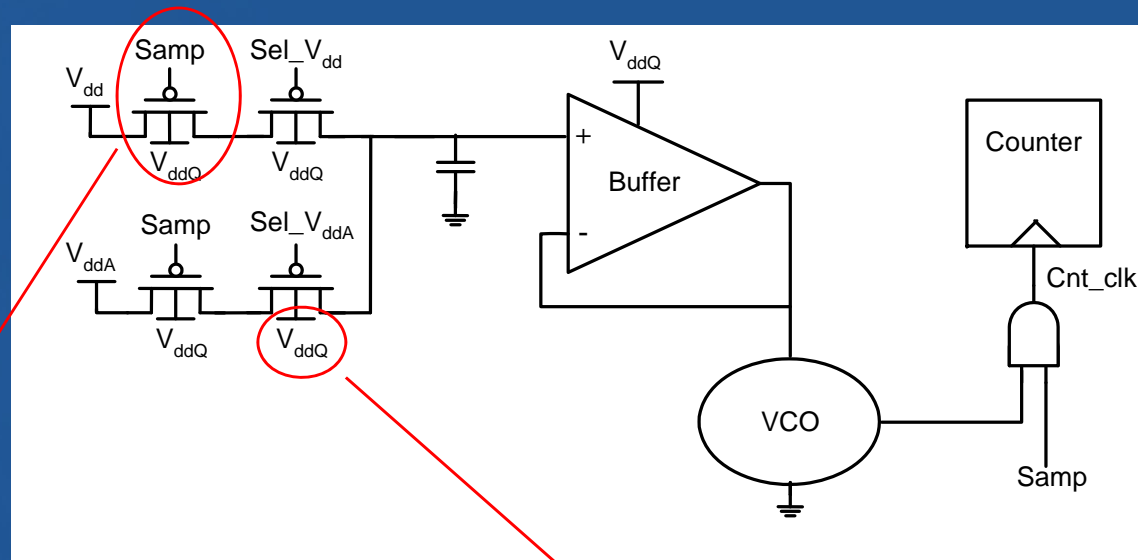
# Measurement Circuits



- External pulse generator controls sampler timing.
- Supply noise on the chip is by definition variation of on-chip  $V_{dd}$  relative to on-chip  $V_{ss}$ .
  - Samplers must be on-chip to avoid reference issues.
- Sampling switches are the only components in the system that are required to have high bandwidth.
- Calibration relaxes linearity and offset requirements of A/D converters.
  - Allows compact and simple on-chip implementation.

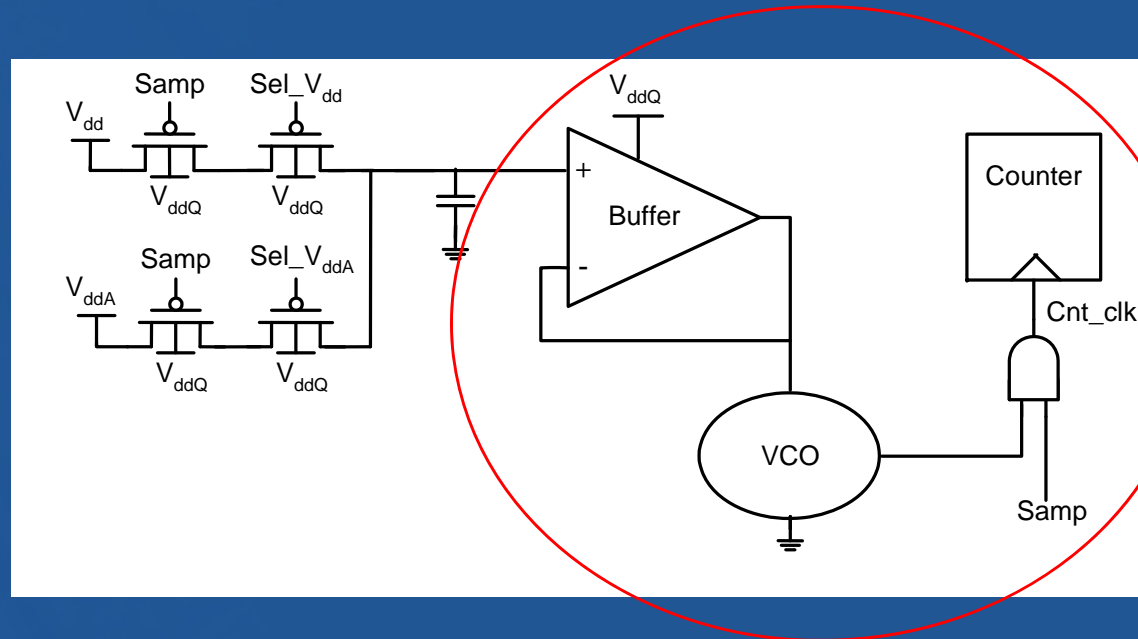


# Sampling switches



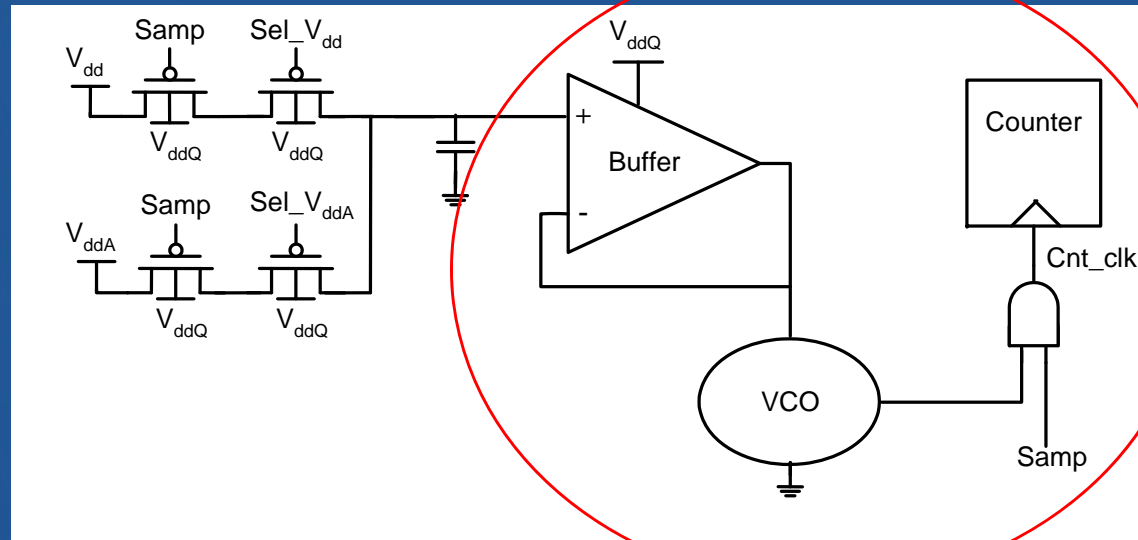
- PMOS switches to achieve required bandwidth.
- Separate, higher than nominal supply
  - $V_{ddQ} = 1.3 \text{ V}$
  - Minimizes coupling between  $V_{dd}$  and sample node during hold.
- Noise on  $V_{ddQ}$  capacitively couples to sample node through switch parasitics.
  - $V_{ddQ}$  heavily decoupled to  $V_{SS}$ .

# VCO Converter



- VCO acts as  $V$ -to- $f$ , clock edge count gives digital estimate of  $f$ .
- $1 \text{ LSB} = 1/(T_{\text{win}} K_{\text{vco}})$
- Measuring **average** VCO frequency – insensitive to high frequency noise.
- Noise on same time scale as counting window unfiltered however.
  - Measurements show that decap + regulator keep  $V_{ddQ}$  well-coupled to on-chip  $V_{ss}$  at these low frequencies.

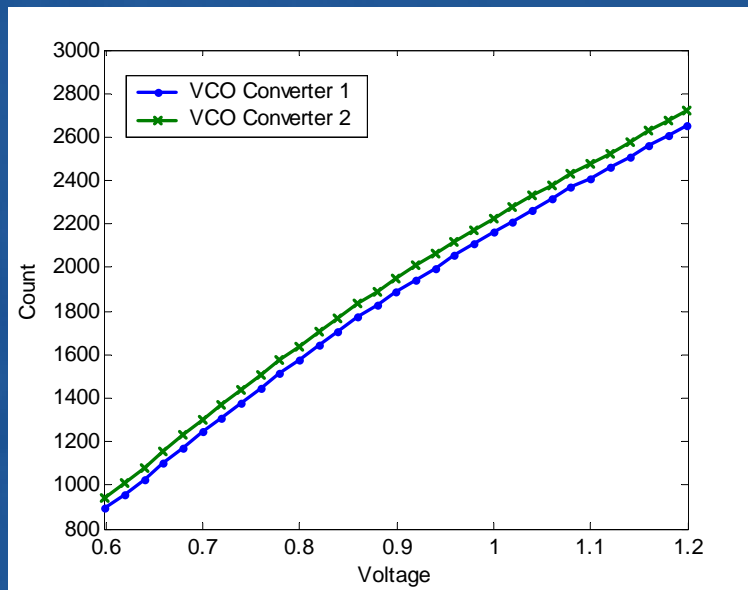
# VCO Converter (cont'd)



- Oscillator phase random w.r.t. counting window
  - Adds uniformly distributed noise with magnitude of 1 LSB.
  - Increases effective resolution with external averaging.
- Multi-phase information from VCO can increase resolution.
  - May be desirable in leaky processes.
- V-to-f curve can vary with temp.
  - Causes gain and/or offset errors
  - Local thermometer (e.g. VCO driven by a relatively constant voltage) can compensate for errors.

# Measurement Results

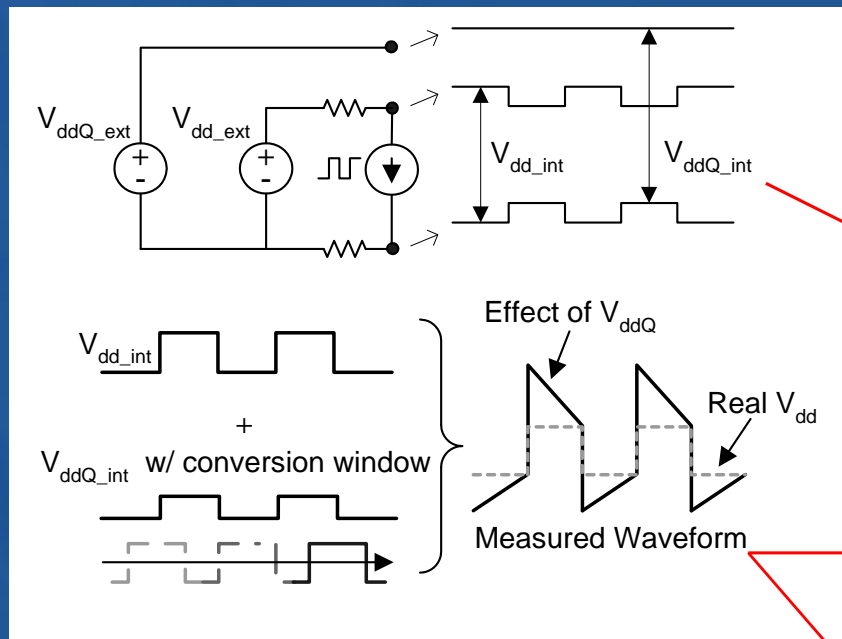
- Measurement circuits implemented in 0.13  $\mu\text{m}$  process with 4 1-10 Gb/s serial links.
  - Can measure digital ( $V_{\text{dd}}$ ) and analog ( $V_{\text{ddA}}$ ) supplies.
  - Noise generators to validate measurement system.



- $K_{\text{VCO}} \approx 2.6 \text{ GHz/V}$
- With 1  $\mu\text{s}$  conversion window:
  - 1 LSB = 385  $\mu\text{V}$

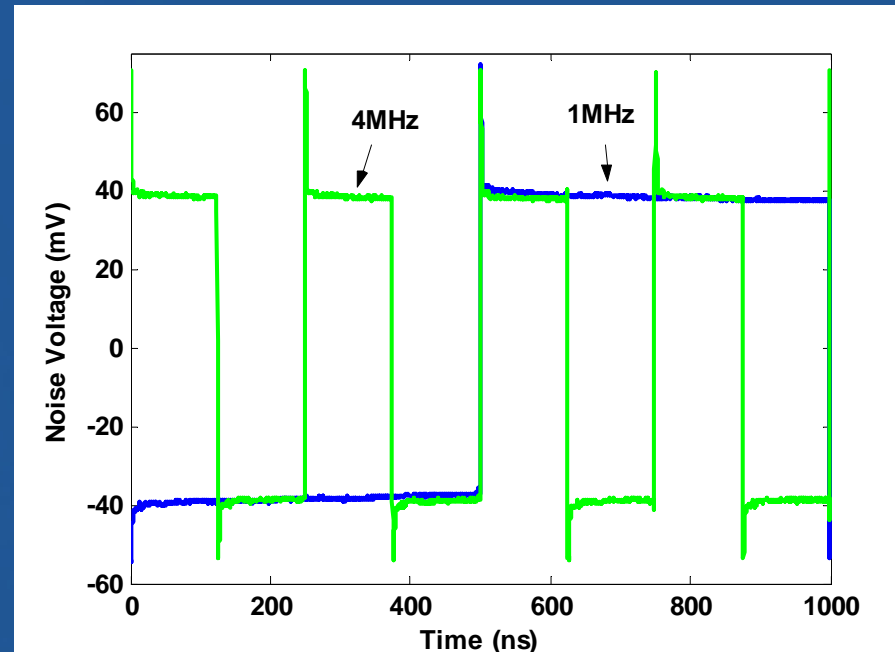
# Measurement System Validation

- Key accuracy concern:
  - Is  $V_{ddQ}$  really quiet at low frequencies?



- Use noise generators to inject square-wave currents onto grid (chip inactive).
  - If  $V_{ddQ}$  not coupled to  $V_{SS}$ ,  $V_{ddQ}$  moves in same direction as  $V_{dd}$ .
- Converter integrates signal
  - If  $T_{win} =$  noise pulse-width, measured waveform (using oscilloscope technique) will have triangular characteristics
  - Height of triangle indicative of  $V_{ddQ}$  noise level.

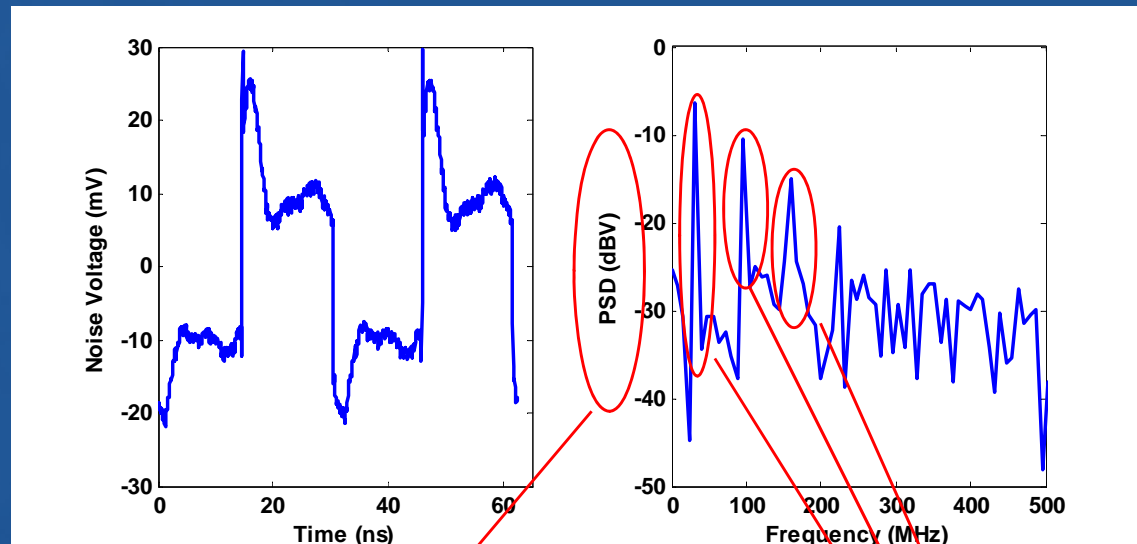
# Measurement System Validation (cont'd)



- Inject noise onto  $V_{ddA}$  at 1 MHz and at 4 MHz
- $T_{\text{in}} = 500 \text{ ns}$
- Height of “triangle” for 1 MHz noise is negligible.
  - $V_{ddQ}$  noise is minimal.

# Autocorrelation Measurement Validation

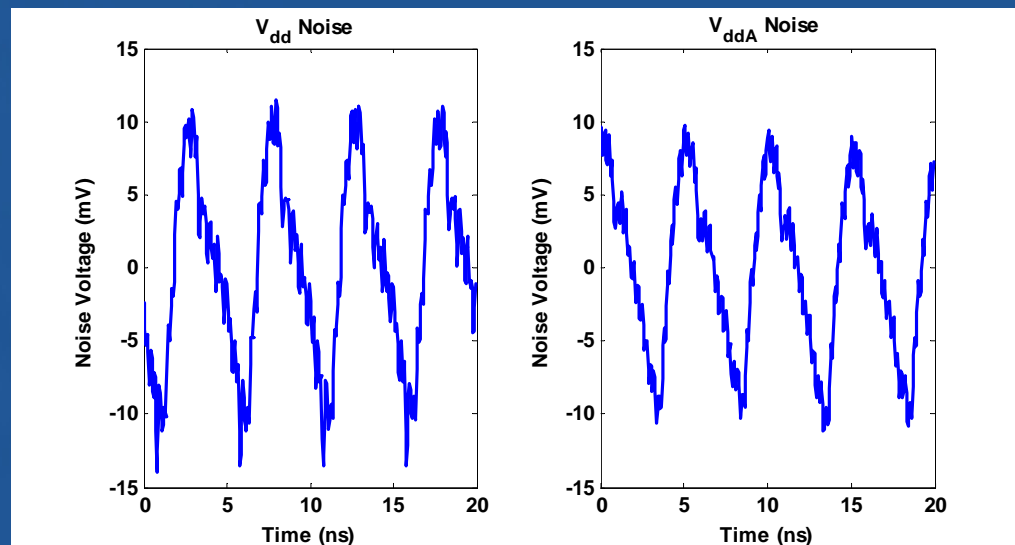
- Inject 32 MHz square noise onto  $V_{dd}$



- PSD scaled by Nyquist frequency to calculate power.
  - Unit: dBV (instead of dB  $V^2/\text{Hz}$ )
  - In dBV, average level roughly corresponds to noise  $\sigma$ .
- Odd harmonics from square waveform

# Measured Supply Noise: Deterministic Noise

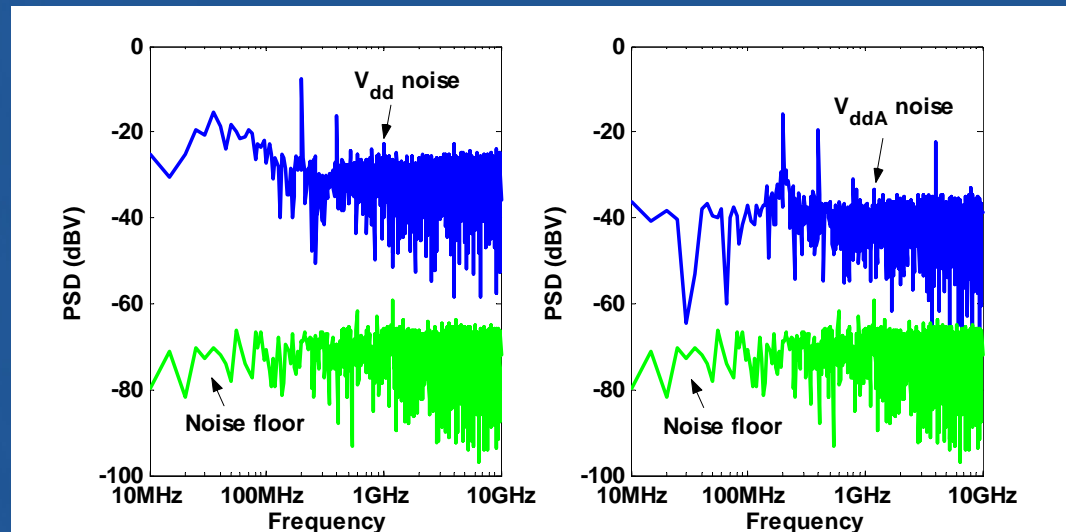
- All 4 links running at 4 Gb/s,  $2^{31}$  PRBS data.
  - Check for deterministic waveform with single sampler.



- 3 major noise frequencies:
  - 200 MHz (ASIC core)
    - Core shares  $V_{SS}$  with links; noise due to ground bounce.
  - 400 MHz (ref clock & some link logic)
  - 4 GHz (data and edge clocks at 2 GHz)



# Measured Supply Noise: Stationary PSD



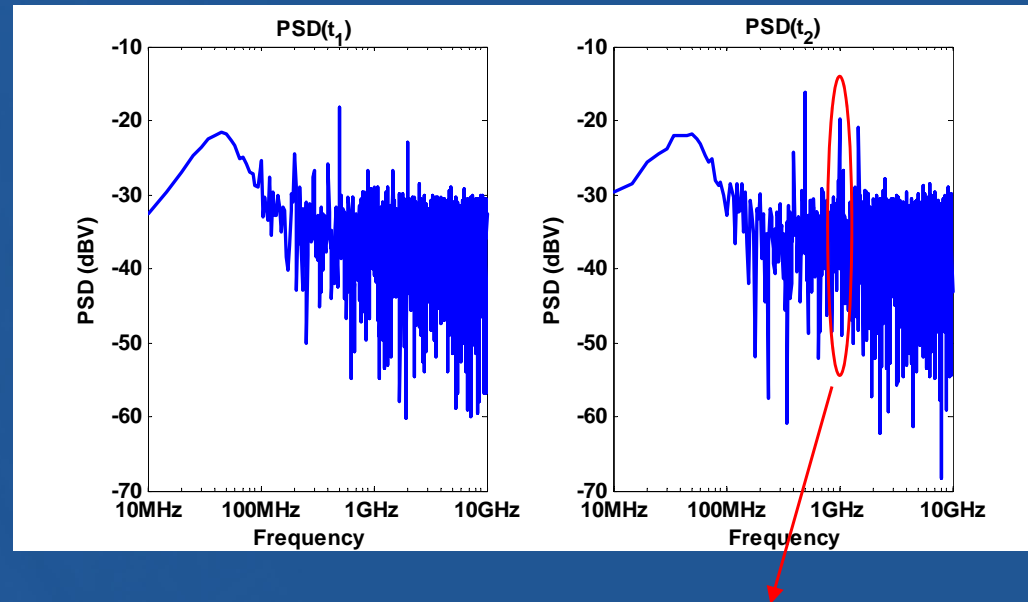
Noise floor measured  
w/chip disabled.

- Engage second sampler and measure stationary (or average) PSD.
  - Deterministic noise dominant.
  - Random noise appears to be white in nature.
- This is the noise that non-periodic circuits will see.
  - Noise appears white b/c it has been time-averaged.

# Cyclostationary Noise

- Cyclostationary noise distribution and PSD are different at each point in time.
  - Measuring PSD at all time points takes extremely large number of samples.
- Measure PSD of random noise at two different times to observe example behavior.
  - Reduce link data-rate to 2 Gb/s to make cyclostationarity more apparent.
    - Majority of logic should complete before the end of the cycle, causing period of relative calm on the power supply.

# Measured Supply Noise: Cyclostationary PSDs



- Measurement verifies cyclostationary behavior.
  - 1 GHz noise at  $t_2$ , but not at  $t_1$ .
- Link clock is 1 GHz for this data-rate
  - Link relatively quiet at  $t_1$ , active at  $t_2$ .

# Conclusions

- **2 low-rate samplers can successfully measure entire frequency spectrum of supply noise.**
  - Low-rate and calibration allow use of simple VCO ADC's for high-resolution measurements.
- **Measured both deterministic and random components of supply noise.**
  - ~20 mV peak-to-peak deterministic noise on both digital and analog supplies.
- **Verified cyclostationarity of random supply noise.**
  - Need to extend modeling techniques for synchronous circuits (e.g. PLLs) to handle cyclostationary noise.
- **Integrated supply noise measurement circuits allow designers to characterize effects of noise on their circuits using real, measured noise spectrums.**